

JCM Proposed Methodology Form

Cover sheet of the Proposed Methodology Form

Form for submitting the proposed methodology

Host Country	Socialist Republic of Viet Nam
Name of the methodology proponents submitting this form	HOYA Corporation
Sectoral scope(s) to which the Proposed Methodology applies	3. Energy demand
Title of the proposed methodology, and version number	Energy Saving by Introduction of High Efficiency Inverter Type Centrifugal Chiller, Version 01.0
List of documents to be attached to this form (please check):	<input type="checkbox"/> The attached draft JCM-PDD: <input checked="" type="checkbox"/> Additional information
Date of completion	07/08/2018

History of the proposed methodology

Version	Date	Contents revised
1.0	07/08/2018	First edition

A. Title of the methodology

Energy Saving by Introduction of High Efficiency Inverter Type Centrifugal Chiller, Version 01.0

B. Terms and definitions

Terms	Definitions
Inverter type centrifugal chiller	An inverter type centrifugal chiller is a chiller which contains inverter, an apparatus to control the speed of the compressor motor in order to maintain the ambient temperature, and includes a centrifugal compressor.
Cooling capacity	The capability of individual chiller to remove heat. In this methodology, “cooling capacity” is used to represent a cooling capacity per one chiller unit and not for a system with multiple chiller units.
Periodical check	A periodical investigation of chiller done by manufacturer or agent who is authorized by the manufacturer, in order to maintain chiller performance.

C. Summary of the methodology

Items	Summary
<i>GHG emission reduction measures</i>	High efficiency centrifugal chiller with inverter technology is introduced to save energy, which leads to GHG emission reductions.
<i>Calculation of reference emissions</i>	Reference emissions are GHG emissions from using reference chiller, calculated with power consumption of project chiller, ratio of COPs (Coefficient Of Performance) of reference/project chillers and CO ₂ emission factor for electricity consumed.
<i>Calculation of project emissions</i>	Project emissions are GHG emissions from using project chiller, calculated with power consumption of project chiller and CO ₂ emission factor for electricity consumed.
<i>Monitoring parameters</i>	<ul style="list-style-type: none"> ● Power consumption of project chiller

	<ul style="list-style-type: none"> ● The amount of fuel consumption and the amount of electricity generated by captive power, where applicable
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D. Eligibility criteria

This methodology is applicable to projects that satisfy all of the following criteria.

Criterion 1	<p>Project chiller is an inverter type centrifugal chiller with a capacity which is less than or equals to 1,500 USRt.</p> <p>*1 USRt = 12,000 BTU/hr = 3.52 kW</p>										
Criterion 2	<p>COP for project chiller i calculated under the standardizing temperature conditions* ($COP_{PJ,tc,i}$) is more than the threshold COP values set in the tables below. (“x” in the table represents cooling capacity per unit.)</p> <table border="1" style="margin: 10px auto;"> <thead> <tr> <th>Cooling capacity per unit (USRt)</th> <th>$300 \leq x < 450$</th> <th>$450 \leq x < 550$</th> <th>$550 \leq x < 825$</th> <th>$825 \leq x \leq 1,500$</th> </tr> </thead> <tbody> <tr> <td>Threshold COP value</td> <td>5.59</td> <td>5.69</td> <td>5.85</td> <td>6.06</td> </tr> </tbody> </table> <p>$COP_{PJ,tc,i}$ is calculated by altering the temperature conditions of COP of project chiller i ($COP_{PJ,i}$) from the project specific conditions to the standardizing conditions. $COP_{PJ,i}$ is derived from specifications prepared for the quotation or factory acceptance test data by manufacturer.</p> <p>[equation to calculate $COP_{PJ,tc,i}$]</p> $COP_{PJ,tc,i} = COP_{PJ,i} \times [(T_{cooling-out,i} - T_{chilled-out,i} + TD_{chilled} + TD_{cooling}) \div (37 - 7 + TD_{chilled} + TD_{cooling})]$ <p>$COP_{PJ,tc,i}$: COP of project chiller i calculated under the standardizing temperature conditions* [-]</p> <p>$COP_{PJ,i}$: COP of project chiller i under the project specific conditions [-]</p> <p>$T_{cooling-out,i}$: Output cooling water temperature of project chiller i set under the project specific conditions [degree Celsius]</p> <p>$T_{chilled-out,i}$: Output chilled water temperature of project chiller i set under the project specific conditions [degree Celsius]</p> <p>$TD_{cooling}$: Temperature difference between condensing temperature of refrigerant and output cooling water temperature, 1.5 degree Celsius set as a default value [degree Celsius]</p>	Cooling capacity per unit (USRt)	$300 \leq x < 450$	$450 \leq x < 550$	$550 \leq x < 825$	$825 \leq x \leq 1,500$	Threshold COP value	5.59	5.69	5.85	6.06
Cooling capacity per unit (USRt)	$300 \leq x < 450$	$450 \leq x < 550$	$550 \leq x < 825$	$825 \leq x \leq 1,500$							
Threshold COP value	5.59	5.69	5.85	6.06							

	<p>TD_{chilled} : Temperature difference between evaporating temperature of refrigerant and output chilled water temperature, 1.5 degree Celsius set as a default value [degree Celsius]</p> <p>*The standardizing temperature conditions to calculate $COP_{PJ,tc,i}$</p> <table> <tr> <td>Chilled water:</td> <td>output</td> <td>7 degrees Celsius</td> </tr> <tr> <td></td> <td>input</td> <td>12 degrees Celsius</td> </tr> <tr> <td>Cooling water:</td> <td>output</td> <td>37 degrees Celsius</td> </tr> <tr> <td></td> <td>input</td> <td>32 degrees Celsius</td> </tr> </table>	Chilled water:	output	7 degrees Celsius		input	12 degrees Celsius	Cooling water:	output	37 degrees Celsius		input	32 degrees Celsius
Chilled water:	output	7 degrees Celsius											
	input	12 degrees Celsius											
Cooling water:	output	37 degrees Celsius											
	input	32 degrees Celsius											
Criterion 3	Periodical check is planned more than one (1) time annually.												
Criterion 4	Ozone Depletion Potential (ODP) of the refrigerant used for project chiller is zero.												
Criterion 5	A plan for prevention of releasing refrigerant used for project chiller is prepared. In the case of replacing the existing chiller with the project chiller, a plan for prevention of releasing refrigerant used in the existing chiller to the air (e.g. re-use of the equipment) is prepared. Execution of this plan is checked at the time of verification, in order to confirm that refrigerant used for the existing one replaced by the project is prevented from being released to the air.												

E. Emission Sources and GHG types

Reference emissions	
Emission sources	GHG types
Power consumption by reference chiller	CO ₂
Project emissions	
Emission sources	GHG types
Power consumption by project chiller	CO ₂

F. Establishment and calculation of reference emissions

F.1. Establishment of reference emissions

Reference emissions are calculated by multiplying power consumption of project chiller, ratio of COPs for reference/project chillers, and CO₂ emission factor for electricity consumed.

The COP of reference chiller is conservatively set as a default value in the following manner to ensure the net emission reductions.

1. The reference COP value varies by its cooling capacity.
2. The maximum values of COP in each cooling capacity range set for this methodology are defined as $COP_{RE,i}$ as described in Section I.

F.2. Calculation of reference emissions

$$RE_p = \sum_i \{ EC_{PJ,i,p} \times (COP_{PJ,tc,i} \div COP_{RE,i}) \times EF_{elec} \}$$

$$COP_{PJ,tc,i} = COP_{PJ,i} \times [(T_{cooling-out,i} - T_{chilled-out,i} + TD_{chilled} + TD_{cooling}) \div (37 - 7 + TD_{chilled} + TD_{cooling})]$$

Where

RE_p	Reference emissions during the period p [tCO ₂ /p]
$EC_{PJ,i,p}$	Power consumption of project chiller i during the period p [MWh/p]
$COP_{PJ,tc,i}$	COP of project chiller i calculated under the standardizing temperature conditions [-]
$COP_{RE,i}$	COP of reference chiller i under the standardizing temperature conditions [-]
EF_{elec}	CO ₂ emission factor for consumed electricity [tCO ₂ /MWh]
$COP_{PJ,i}$	COP of project chiller i under the project specific conditions [-]
$T_{cooling-out,i}$	Output cooling water temperature of project chiller i set under the project specific conditions [degree Celsius]
$T_{chilled-out,i}$	Output chilled water temperature of project chiller i set under the project specific conditions [degree Celsius]
$TD_{chilled}$	Temperature difference between condensing temperature of refrigerant and output cooling water temperature, 1.5 degree Celsius set as a default value [degree Celsius]
$TD_{cooling}$	Temperature difference between evaporating temperature of refrigerant and output chilled water temperature, 1.5 degree Celsius set as a default value [degree Celsius]
i	Identification number of project chiller

G. Calculation of project emissions

$$PE_p = \sum_i (EC_{PJ,i,p} \times EF_{elec})$$

Where

PE_p	Project emissions during the period p [tCO ₂ /p]
$EC_{PJ,i,p}$	Power consumption of project chiller i during the period p [MWh/p]
EF_{elec}	CO ₂ emission factor for consumed electricity [tCO ₂ /MWh]

H. Calculation of emissions reductions

$$ER_p = RE_p - PE_p$$

Where

ER_p	Emission reductions during the period p [tCO ₂ /p]
RE_p	Reference emissions during the period p [tCO ₂ /p]
PE_p	Project emissions during the period p [tCO ₂ /p]

I. Data and parameters fixed *ex ante*

The source of each data and parameter fixed *ex ante* is listed as below.

Parameter	Description of data	Source
EF_{elec}	CO ₂ emission factor for consumed electricity. When project chillers consume only grid electricity or captive electricity, the project participant applies the CO ₂ emission factor respectively. When project chillers may consume both grid electricity and captive electricity, the project participant applies the CO ₂ emission factor with lower value.	[Grid electricity] Ministry of Natural Resources and Environment of Vietnam (MONRE), Vietnamese DNA for CDM unless otherwise instructed by the Joint Committee. [Captive electricity] For the option a) Specification of the captive power generation system

	<p>[CO₂ emission factor]</p> <p>For grid electricity: The most recent value available from the source stated in this table at the time of validation</p> <p>For captive electricity, it is determined based on the following options:</p> <p>a) Calculated from its power generation efficiency ($\eta_{\text{elec,CG}}$ [%]) obtained from manufacturer's specification</p> <p>The power generation efficiency based on lower heating value (LHV) of the captive power generation system from the manufacturer's specification is applied;</p> $EF_{\text{elec}} = 3.6 \times \frac{100}{\eta_{\text{elec,CG}}} \times EF_{\text{fuel,CG}}$ <p>b) Calculated from measured data</p> <p>The power generation efficiency calculated from monitored data of the amount of fuel input for power generation ($FC_{\text{PJ,CG,p}}$) and the amount of electricity generated ($EG_{\text{PJ,CG,p}}$) during the monitoring period p is applied. The measurement is conducted with the monitoring equipment to which calibration certificate is issued by an entity accredited under national/international standards;</p> $EF_{\text{elec}} = FC_{\text{PJ,CG,p}} \times NCV_{\text{fuel,CG}} \times EF_{\text{fuel,CG}} \times \frac{1}{EG_{\text{PJ,CG,p}}}$ <p>Where:</p> <p>$NCV_{\text{fuel,CG}}$: Net calorific value of fuel consumed by the captive power generation system [GJ/mass or volume]</p> <p>Note:</p> <p>In case the captive electricity generation system</p>	<p>provided by the manufacturer ($\eta_{\text{elec,CG}}$ [%]).</p> <p>CO₂ emission factor of the fossil fuel type used in the captive power generation system ($EF_{\text{fuel,CG}}$ [tCO₂/GJ])</p> <p>For the option b)</p> <p>Generated and supplied electricity by the captive power generation system ($EG_{\text{PJ,CG,p}}$ [MWh/p]).</p> <p>Fuel amount consumed by the captive power generation system ($FC_{\text{PJ,CG,p}}$ [mass or volume/p]).</p> <p>Net calorific value ($NCV_{\text{fuel,CG}}$ [GJ/mass or volume]) and CO₂ emission factor ($EF_{\text{fuel,CG}}$ [tCO₂/GJ]) of the fuel consumed by the captive power generation system in order of preference:</p> <ol style="list-style-type: none"> 1) values provided by the fuel supplier; 2) measurement by the project participants; 3) regional or national default values; 4) IPCC default values provided in tables 1.2 and 1.4 of Ch.1 Vol.2 of 2006 IPCC Guidelines on National GHG Inventories. Lower value is applied.
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	<p>meets all of the following conditions, the value in the following table may be applied to EF_{elec} depending on the consumed fuel type.</p> <ul style="list-style-type: none"> ● The system is non-renewable generation system ● Electricity generation capacity of the system is less than or equal to 15 MW <table border="1" data-bbox="427 658 963 826"> <thead> <tr> <th>fuel type</th> <th>Diesel fuel</th> <th>Natural gas</th> </tr> </thead> <tbody> <tr> <td>EF_{elec}</td> <td>0.8 *₁</td> <td>0.46 *₂</td> </tr> </tbody> </table> <p>*1 The most recent value at the time of validation is applied. *2 The value is calculated with the equation in the option a) above. The lower value of default effective CO₂ emission factor for natural gas (0.0543 tCO₂/GJ), and the most efficient value of default efficiency for off-grid gas turbine systems (42%) are applied.</p>	fuel type	Diesel fuel	Natural gas	EF_{elec}	0.8 * ₁	0.46 * ₂	<p>[Captive electricity with diesel fuel] CDM approved small scale methodology: AMS-I.A.</p> <p>[Captive electricity with natural gas] 2006 IPCC Guidelines on National GHG Inventories for the source of EF of natural gas. CDM Methodological tool "Determining the baseline efficiency of thermal or electric energy generation systems version02.0" for the default efficiency for off-grid power plants.</p>				
fuel type	Diesel fuel	Natural gas										
EF_{elec}	0.8 * ₁	0.46 * ₂										
<p>$COP_{RE,i}$</p>	<p>COP of reference chiller i under the standardizing temperature conditions</p> <p>The COP of the reference chiller i is selected from the default COP value in the following table in line with cooling capacity of the project chiller i. ("x" in the table represents cooling capacity per unit.)</p> <table border="1" data-bbox="422 1736 968 1921"> <thead> <tr> <th>Cooling capacity per unit (USRt)</th> <th>300≤x<450</th> <th>450≤x<550</th> <th>550≤x<825</th> <th>825<x≤1,500</th> </tr> </thead> <tbody> <tr> <td>$COP_{RE,i}$</td> <td>5.59</td> <td>5.69</td> <td>5.85</td> <td>6.06</td> </tr> </tbody> </table>	Cooling capacity per unit (USRt)	300≤x<450	450≤x<550	550≤x<825	825<x≤1,500	$COP_{RE,i}$	5.59	5.69	5.85	6.06	<p>Specifications of project chiller i prepared for the quotation or factory acceptance test data by manufacturer.</p> <p>The default COP values are derived from the result of survey on COP of chillers from manufacturers that have high market share. The survey should prove the use of clear methodology. The default COP values should be</p>
Cooling capacity per unit (USRt)	300≤x<450	450≤x<550	550≤x<825	825<x≤1,500								
$COP_{RE,i}$	5.59	5.69	5.85	6.06								

	*1 USRt = 12,000 BTU/hr = 3.52 kW	revised if necessary from survey result which is conducted by JC or project participants.
$COP_{P,i}$	The COP of project chiller i under the project specific conditions.	Specifications of project chiller i prepared for the quotation or factory acceptance test data by manufacturer
$T_{cooling-out,i}$	Output cooling water temperature of project chiller i set under the project specific conditions.	Specifications of project chiller i prepared for the quotation or factory acceptance test data by manufacturer
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