Joint Crediting Mechanism Approved Methodology TH_AM011 "Installation of Energy-efficient Refrigerators Using Natural Refrigerant at Cold Storage"

A. Title of the methodology

Installation of Energy-efficient Refrigerators Using Natural Refrigerant at Cold Storage, Version 01.0

B. Terms and definitions

| Terms | Definitions |
|-------------------------------|--|
| Secondary loop cooling system | A secondary loop cooling system is an indirect cooling |
| | system that cools the object with a secondary refrigerant |
| | (e.g., brine) which is cooled by a primary refrigerant (e.g., |
| | HFC). The secondary loop cooling system primarily consists |
| | of the refrigerator which is mainly composed of the |
| | compressor and heat exchangers as the primary refrigeration |
| | cycle and pumps, heat exchangers and fans as the secondary |
| | refrigeration cycle. |
| | The secondary loop cooling system is described as "primary |
| | refrigerant/secondary refrigerant" (e.g., "HFC/brine"). |
| Coefficient of Performance | COP is defined as a value calculated by dividing refrigeration |
| (COP) | capacity by electricity consumption of a refrigerator under a |
| | full load condition. Electricity consumption of a refrigerator |
| | is defined in this methodology as the electricity used to |
| | operate the compressor. Electricity consumption of pumps for |
| | circulating the secondary refrigerant, and other ancillary |
| | equipment are not included in the COP calculation. |
| | |
| | The room temperature conditions at which COPs are |
| | calculated in this methodology are shown below: |
| | • Room temperature condition: - 25 deg. C, 0 deg. C, 5 |
| | deg. C |
| | • Cooling water fed to condenser: inlet 32 deg. C |
| Natural refrigerant | Natural refrigerant refers to naturally occurring substances |

| | with refrigeration capacity and with zero ozone depletion | |
|------------------|--|--|
| | potential (ODP) (e.g. CO ₂ and NH ₃). | |
| Periodical check | Periodical check is a periodical maintenance operation done | |
| | by the manufacturer or an agent who is authorized by the | |
| | manufacturer to maintain refrigerator performance (not | |
| | including part replacement or overhaul). | |

C. Summary of the methodology

| Items | Summary | | |
|--------------------------|---|--|--|
| GHG emission reduction | Energy-efficient refrigerators using natural refrigerant is | | |
| measures | introduced for energy saving at the cold storage. | | |
| Calculation of reference | Reference emissions are GHG emissions from reference | | |
| emissions | refrigerators, calculated by using data of power consumption of | | |
| | project refrigerator, ratio of COPs of reference/project | | |
| | refrigerators and CO ₂ emission factor for consumed electricity. | | |
| Calculation of project | Project emissions are GHG emissions from project refrigerator, | | |
| emissions | calculated with power consumption of project refrigerator and | | |
| | CO ₂ emission factor for consumed electricity. | | |
| Monitoring parameters | Power consumption of project refrigerator | | |

D. Eligibility criteria

This methodology is applicable to projects that satisfy all of the following criteria.

| Criterion 1 | Refrigerator(s) with a secondary loop cooling system using CO ₂ as a refrigerant | | | | | |
|-------------|---|--------------------------------------|-----------------------|------|--|--|
| | and equipped with inve | erter is installed at cold storage. | | | | |
| Criterion 2 | COP of project refriger | rator(s) installed in the project co | ooling system is more | than | | |
| | the threshold COP values set in the tables below. ("x" in the table represents | | | | | |
| | cooling capacity per unit.) | | | | | |
| | Room temperature Cooling capacity Threshold COP | | | | | |
| | condition | value | | | | |
| | - 25 deg. C $42.4 \le x \le 340.0$ 1.71 | | | | | |
| | 0 deg. C $73.6 \le x \le 516.4$ 2.79 | | | | | |
| | 5 deg. C $86.2 \le x \le 612.6$ 3.20 | | | | | |
| | · | | | | | |

| | COP for the project refrigerator(s) are calculated with the following conditions: | | |
|-------------|---|--|--|
| | • Room temperature condition: - 25 deg. C or 0 deg. C or 5 deg. C | | |
| | Cooling water fed to condenser: inlet 32 deg. C | | |
| Criterion 3 | Periodical check is planned at least one (1) time annually. | | |
| Criterion 4 | In the case of replacing the existing refrigerator with the project refrigerator, a | | |
| | plan for prevention of releasing refrigerant used in the existing refrigerator to the | | |
| | air (e.g. re-use of the equipment) is prepared. Execution of this plan is checked at | | |
| | the time of verification, in order to confirm that refrigerant used for the existing | | |
| | one replaced by the project is prevented from being released to the air. | | |

E. Emission Sources and GHG types

| Reference emissions | | | |
|---|-----------------|--|--|
| Emission sources GHG types | | | |
| Power consumption by the reference refrigerator | CO ₂ | | |
| Project emissions | | | |
| Emission sources | GHG types | | |
| Power consumption by the project refrigerator | CO ₂ | | |

F. Establishment and calculation of reference emissions

F.1. Establishment of reference emissions

Reference emissions are calculated by multiplying the power consumption of project refrigerator, ratio of COPs for reference/project refrigerators and CO₂ emission factor for consumed electricity.

The following types of cooling system are identified as possible cooling systems other than the project system to be installed at cold storage:

• For room temperature condition of -25 deg. C: HFC dry expansion (single loop), NH₃ flooded, pump system (single loop), HFC/brine (secondary loop) and NH₃/brine (secondary loop)

• For room temperature condition of 0 deg. C and 5 deg. C: HFC dry expansion (single loop) This methodology ensures that net emission reductions are achieved by applying the following conservative assumptions: • Determination of default values for COP_{RE}:

The maximum COP values of refrigerators among the data of possible type cooling systems available in Thai market within the range specified by Criterion 2 is defined as the default values of COP_{RE} (1.71 for temperature condition of - 25 deg. C, 2.79 for temperature condition of 0 deg. C and 3.20 for 5 deg. C) to ensure the net emission reductions.

• Emissions associated with leakage of refrigerant in operation:

Among the possible types of cooling systems, two cooling systems use HFCs (R404A, GWP: 3,000-4,000) as refrigerant. The project cooling system uses a natural refrigerant that has a very small GWP (CO₂: 1, NH₃: less than 1). However, emissions associated with leakage of refrigerant are not counted in the emission reduction calculation.

• Project refrigerator equipped with inverter:

The project refrigerator is controlled by inverter technology. In this methodology, COP is defined under the condition of full load although in reality a cold storage is often operated under the condition of partial load where the efficiency of the refrigerator without inverter tends to decrease because of its intermittent operation. Calculating emissions based on the COPs of full load conditions is deemed conservative since the efficiency of the project refrigerator is likely to be maintained either at the full load or at partial load condition as it is equipped with inverter.

F.2. Calculation of reference emissions

$$RE_p = \sum_{i} \left(EC_{PJ,i,p} \times \frac{COP_{PJ,i}}{COP_{RE,i}} \times EF_{elec} \right)$$

Where

| wnere | |
|----------------------|--|
| RE_p | Reference emissions during the period p [tCO ₂ /p] |
| EC _{PJ,i,p} | Power consumption of project refrigerator i during the period p [MWh/p] |
| COP _{PJ,i} | COP of project refrigerator <i>i</i> [-] |
| $COP_{RE,i}$ | COP of reference refrigerator <i>i</i> [-] |
| EF _{elec} | CO ₂ emission factor for consumed electricity [tCO ₂ /MWh] |
| i | Identification number of refrigerators |
| | |

G. Calculation of project emissions

$$PE_p = \sum_{i} (EC_{PJ,i,p} \times EF_{elec})$$

Where

| PE_p | Project emissions during the period p [tCO ₂ /p] |
|--------------------|--|
| $EC_{PJ,i,p}$ | Power consumption of project refrigerator i during the period p [MWh/p] |
| EF _{elec} | CO ₂ emission factor for consumed electricity [tCO ₂ /MWh] |
| i | Identification number of refrigerators |

H. Calculation of emissions reductions

| | $ER_p = RE_p - PE_p$ |
|--------|---|
| Where | |
| ER_p | Emission reductions during the period p [tCO ₂ /p] |
| RE_p | Reference emissions during the period p [tCO ₂ /p] |
| PE_p | Project emissions during the period p [tCO ₂ /p] |
| | |

I. Data and parameters fixed *ex ante*

The source of each data and parameter fixed *ex ante* is listed as below.

| Parameter | Description of data | Source |
|---------------------|---|--|
| COP _{PJ,i} | COP of project refrigerator <i>i</i> [-]. | Specifications of project |
| | | refrigerator <i>i</i> prepared for the |
| | The room temperature conditions at which COPs | quotation or factory |
| | are calculated in this methodology are shown | acceptance test data at the |
| | below: | time of shipment by |
| | • Room temperature condition: - 25 deg. C, 0 | manufacturer. |
| | deg. C, 5 deg. C | |
| | • Cooling water fed to condenser: inlet 32 | |
| | deg. C | |

| COP _{RE,i} | COP of reference refrigerator <i>i</i> [-] | | | | The default COP values are |
|---------------------|---|--------------------|--------------------------|------------------------------|---|
| | | | | | derived from the maximum |
| | The default values for $COP_{RE,i}$ is applied | | | | value of COP among the |
| | depending on the room temperature condition set | | | | available data of the possible |
| | for the project refrigerator <i>i</i> : | | | | types of refrigerators except |
| | Temperature | Cooling | project within the range | | |
| | condition | capacity | values | | specified by Criterion 2. |
| | - 25 deg. C | $42.4 \leq x \leq$ | 1.71 | | The survey should prove the |
| | | 340.0kW | | | use of clear methodology. |
| | 0 deg. C | $73.6 \le x \le$ | 2.79 | | Default values of $COP_{RE,i}$ |
| | | 516.4kW | | | should be revised if |
| | 5 deg. C | $86.2 \le x \le$ | 3.20 | | necessary from survey result |
| | | 612.6kW | | | which is conducted by JC or |
| | * "x" in the tabl | e represents co | oling capacity p | er | project participants. |
| | unit. | | | | |
| EF _{elec} | CO ₂ emission | factor for con | sumed electric | ity | Case 1) |
| | [tCO ₂ /MWh]. | | | | [Grid electricity] |
| | When the project refrigerator consumes only 1) | | | | The most recent value |
| | grid electricity, 2) captive electricity or 3) | | | | available at the time of |
| | electricity directly supplied from other sources | | | | validation is applied and fixed |
| | (e.g. independent power producer (IPP), small | | | | for the monitoring period |
| | power producer (SPP) and very small power | | | | thereafter. The data is sourced |
| | producer (VSPP)) to the project site, the project | | | | from "Grid Emission Factor |
| | participant app | blies the CO_2 | tor | (GEF) of Thailand", endorsed | |
| | respectively. | | | | by Thailand Greenhouse Gas |
| | When the pro- | ject refrigerate | or may consum | me | Management Organization |
| | electricity supp | olied from mor | e than 1 elect | ric | (TGO) unless otherwise |
| | source, the pro- | | | O_2 | instructed by the Joint |
| | emission factor with the lowest value. | | | | Committee. |
| | [CO ₂ emission factor] | | | | Case 2) |
| | Case 1) Grid electricity | | | | [Captive electricity] |
| | The most recent value available from the source | | | | For Option a) |
| | stated in this table at the time of validation | | | | Specification of the captive |
| | | | | | power generation system |
| | Case 2) Captive electricity including | | | | provided by the manufacturer |
| | cogeneration system | | | | $(\eta_{elec}$ [%]). CO ₂ emission |
| <u> </u> | | | | | |

 EF_{elec} is determined based on the following options:

a) <u>Calculated from its power generation</u>
<u>efficiency (η_{elec} [%]) obtained from</u>
<u>manufacturer's specification.</u>

The power generation efficiency based on lower heating value (LHV) of the captive power generation system from the manufacturer's specification is applied;

$$EF_{gen} = 3.6 \times \frac{100}{\eta_{elec}} \times EF_{fuel}$$

b) Calculated from measured data

The power generation efficiency calculated from monitored data of the amount of fuel input for power generation ($FC_{PJ,p}$) and the amount of electricity generated ($EG_{PJ,p}$) during the period pis applied. The measurement is conducted with the monitoring equipment to which calibration certificate is issued by an entity accredited under national/international standards;

$$EF_{elec} = FC_{PJ,p} \times NCV_{fuel} \times EF_{fuel} \times \frac{1}{EG_{PJ,p}}$$

Where:

NCV_{fuel} : Net calorific value of consumed fuel [GJ/mass or volume]

Note:

In case the captive electricity generation system meets all of the following conditions, the value in the following table may be applied to EF_{elec} depending on the consumed fuel type.

- The system is non-renewable generation system
- Electricity generation capacity of the system is less than or equal to 15 MW

factor of the fossil fuel type used in the captive power generation system (EF_{fuel} [tCO₂/GJ])

For Option b)

Generated supplied and electricity by the captive power generation system $(EG_{PI,p} [MWh/p]).$ Fuel amount consumed by the captive power generation system (FC_{PLp}) [mass or volume/p]). Net calorific value (NCV_{fuel} [GJ/mass or volume]) and CO₂ emission factor of the fuel (EF_{fuel} [tCO₂/GJ]) in order of preference: 1) values provided by the fuel supplier; 2) measurement by the project participants; 3) regional or national default values; 4) IPCC default values provided in tables 1.2 and 1.4 of Ch.1 Vol.2 of 2006 IPCC Guidelines on National GHG Inventories. Lower value is applied. [Captive electricity with diesel fuel] CDM approved small scale

[Captive electricity with natural gas]

methodology: AMS-I.A.

| fuel type | Diesel fuel | Natural gas | 2006 IPCC Guidelines on |
|--|-----------------------|---|---------------------------------|
| EF _{elec} | 0.8 *1 | 0.46 *2 | National GHG Inventories |
| *1 The most re | ecent value at the | for the source of EF of | |
| validation is a | pplied. | natural gas. | |
| *2 The value i | s calculated with the | CDM Methodological tool | |
| option a) abo | ove. The lower | value of default | "Determining the baseline |
| effective CO2 | emission factor | for natural gas | efficiency of thermal or |
| (0.0543tCO ₂ /0 | GJ), and the most | efficient value of | electric energy generation |
| default efficient | ncy for off-grid ga | s turbine systems | systems version 02.0" for the |
| (42%) are app | lied. | | default efficiency for off-grid |
| | | power plants. | |
| Case 3) Elect | ricity directly sup | | |
| other sources | including cogene | Case 3) [Electricity directly supplied from other sources including | |
| EF_{elec} is dete | rmined based on t | | |
| options: | | cogeneration system] | |
| a) The value p | rovided by the ele | For Option a) | |
| with the evide | nce; | The evidence stating | |
| b) The value c | alculated in the sa | me manner for | information relevant to the |
| the option a) o | f 2) captive electric | icity as | value of emission factor (e.g. |
| instructed abo | ve; | | data of power generation, type |
| c) The value c | alculated in the sa | me manner for | of power plant, type of fossil |
| the option b) of 2) captive electricity as | | | fuel, period of time). |
| instructed above; | | | |
| When the pr | roject refrigerator | | |
| electricity sup | plied from more | | |
| source, the pr | roject participant | | |
| emission facto | r with the lowest | value. | |

History of the document

| Version | Date | Contents revised |
|---------|-------------------|--|
| 01.0 | 20 September 2021 | Electronic decision by the Joint Committee |
| | | Initial approval. |
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