## JCM Proposed Methodology Form

# Cover sheet of the Proposed Methodology Form

Form for submitting the proposed methodology

| Host Country                                  | Kingdom of Cambodia                         |  |  |
|---|---|--|--|
| Name of the methodology proponents            | AEON MALL Co., Ltd.                         |  |  |
| submitting this form                          |   |  |  |
| Sectoral scope(s) to which the Proposed       | 3.Energy demand                             |  |  |
| Methodology applies                           |   |  |  |
| Title of the proposed methodology, and        | Introduction of High Efficiency Centrifugal |  |  |
| version number                                | Chiller, Ver01.0                            |  |  |
| List of documents to be attached to this form | The attached draft JCM-PDD:                 |  |  |
| (please check):                               | Additional information                      |  |  |
| Date of completion                            | 14/11/2018                                  |  |  |

History of the proposed methodology

| Version | Date       | Contents revised |
|---------|------------|------------------|
| 1.0     | 14/11/2018 | First edition    |
|         |            |                  |
|         |            |                  |

# A. Title of the methodology

Introduction of High Efficiency Centrifugal Chiller, Ver01.0

# **B.** Terms and definitions

| Terms               | Definitions  |  |  |  |
|---------------------|--|--|--|--|
| Centrifugal chiller | A centrifugal chiller is a chiller applying a centrifugal          |  |  |  |
|                     | compressor. It is commonly used for air-conditioning with huge     |  |  |  |
|                     | cooling load, e.g., buildings, shopping malls or factories etc.    |  |  |  |
| Cooling capacity    | Cooling capacity is the ability of individual chiller to remove    |  |  |  |
|                     | heat. In this methodology, "cooling capacity" is used to represent |  |  |  |
|                     | a cooling capacity per one chiller unit and not for a system with  |  |  |  |
|                     | multiple chiller units.  |  |  |  |
| Periodical check    | Periodical check is a periodical investigation of chiller done by  |  |  |  |
|                     | manufacturer or agent who is authorized by the manufacturer, in    |  |  |  |
|                     | order to maintain chiller performance.                             |  |  |  |

# C. Summary of the methodology

| Items                    | Summary  |  |  |
|--------------------------|--|--|--|
| GHG emission reduction   | High efficiency centrifugal chiller is introduced to save energy,        |  |  |
| measures                 | which leads to GHG emission reductions.                                  |  |  |
| Calculation of reference | Reference emissions are GHG emissions from using reference               |  |  |
| emissions                | chiller, calculated with power consumption of project chiller,           |  |  |
|                          | ratio of COPs (Coefficient Of Performance) of reference/project          |  |  |
|                          | chillers and CO <sub>2</sub> emission factor for electricity consumed.   |  |  |
| Calculation of project   | Project emissions are GHG emissions from using project chiller,          |  |  |
| emissions                | calculated with power consumption of project chiller and CO <sub>2</sub> |  |  |
|                          | emission factor for electricity consumed.                                |  |  |
| Monitoring parameters    | Power consumption of project chiller                                     |  |  |
|                          | • Amount of fuel consumed and amount of electricity                      |  |  |
|                          | generated by captive power, where applicable.                            |  |  |

| D. Eligibility criteria  |   |                        |                      |   |  |                                 |
|--|---|------------------------|----------------------|---|--|---------------------------------|
| This methodology is applicable to projects that satisfy all of the following criteria. |   |                        |                      |   |  |                                 |
| Criterion 1  | Project chiller is a centrifugal chiller with a capacity of less than or equal to                           |                        |                      |   | than or equal to   |                                 |
|  | 1,300 USRt.   |                        |                      |   |  |                                 |
|  | * 1 USRt = 3.52 l   | κW                     |                      |   |  |                                 |
| Criterion 2  | COP for project   | t chil                 | ler <i>i</i> calcula | ted under th  | ne standardizi   | ing temperature                 |
|  | conditions* (COI  | P <sub>PJ,tc,i</sub> ) | is more than         | the threshold   | COP values   | set in the tables               |
|  | below. ("x" in the  | table                  | represents co        | oling capacity  | per unit.)   |                                 |
|  |   |                        |                      |   |  |                                 |
|  | [Threshold COP  | values                 | for project ch       | iller]  | 1  |                                 |
|  | Cooling capacity<br>unit (USRt)   | y per                  | 300≤x≤350            | 350 <x≤550< th=""><th>550<x≤750< th=""><th>750<x≤1,300< th=""></x≤1,300<></th></x≤750<></th></x≤550<> | 550 <x≤750< th=""><th>750<x≤1,300< th=""></x≤1,300<></th></x≤750<> | 750 <x≤1,300< th=""></x≤1,300<> |
|  | Threshold COP v   | alue                   | 5.46                 | 5.76  | 5.90   | 6.03                            |
|  |   |                        | I                    |   |  | II                              |
|  | COP <sub>PJ,tc,i</sub> is a re  | calcul                 | lation of CO         | P of project  | chiller i (Co  | $OP_{PJ,i}$ ) adjusting         |
|  | temperature cond  | itions                 | from the proj        | ect specific c  | onditions to t   | he standardizing                |
|  | conditions. $\text{COP}_{\text{PJ},i}$ is derived from specifications prepared for the quotation or         |                        |                      |   |  |                                 |
|  | factory acceptance test data at the time of shipment by manufacturer.                                       |                        |                      |   |  |                                 |
|  | [equation to calculate COP <sub>PJ,tc,i</sub> ]   |                        |                      |   |  |                                 |
|  | $COP_{PJ,tc,i} = COP_{PJ,i} \times [(T_{cooling-out,i} - T_{chilled-out,i} + TD_{chilled} + TD_{cooling})]$ |                        |                      |   |  |                                 |
|  | $\div (37 - 7 + TD_{chilled} + TD_{cooling})]$  |                        |                      |   |  |                                 |
|  | cooling/1   |                        |                      |   |  |                                 |
|  | $COP_{PJ,tc,i}$ : COP of project chiller <i>i</i> calculated under the standardizing                        |                        |                      |   |  |                                 |
|  | temperature conditions* [-]   |                        |                      |   | _  |                                 |
|  | $COP_{PI,i}$ : COP of project chiller <i>i</i> under the project specific conditions                        |                        |                      |   |  |                                 |
|  | [-]   |                        |                      |   |  |                                 |
|  | $T_{cooling-out,i}$ : Output cooling water temperature of project chiller <i>i</i> set                      |                        |                      |   |  |                                 |
|  | under the project specific condition [degree Celsius]   |                        |                      |   |  |                                 |
|  | $T_{chilled-out,i}$ : Output chilled water temperature of project chiller <i>i</i> set                      |                        |                      |   |  |                                 |
|  | under the project specific condition [degree Celsius]   |                        |                      |   |  |                                 |
|  | TD <sub>cooling</sub> : Temperature difference between condensing temperature of                            |                        |                      |   |  |                                 |
|  | refrigerant and output cooling water temperature 1.5 degrees  |                        |                      |   |  |                                 |
|  |   | Celsiu                 | us set as a defa     | ault value [deg   | gree Celsius]  |                                 |

|             | TD <sub>chilled</sub> : Temperature difference between evaporating temperature of   |  |  |  |
|-------------|---|--|--|--|
|             | refrigerant and output chilled water temperature, 1.5 degrees   |  |  |  |
|             | Celsius set as a default value [degree Celsius]   |  |  |  |
|             | *The standardizing temperature conditions to calculate COP <sub>PJ,tc,i</sub><br>Chilled water: output 7 degrees Celsius<br>input 12 degrees Celsius<br>Cooling water: output 37 degrees Celsius<br>input 32 degrees Celsius  |  |  |  |
| Criterion 3 | Periodical check is planned more than one (1) time annually.  |  |  |  |
| Criterion 4 | Ozone Depletion Potential (ODP) of the refrigerant used for project chiller is zero.  |  |  |  |
| Criterion 5 | A plan for prevention of releasing refrigerant used for project chiller is prepared.<br>In the case of replacing the existing chiller with the project chiller, a plan for<br>prevention of releasing refrigerant used in the existing chiller to the air (e.g.<br>re-use of the equipment) is prepared. Execution of this plan is checked at the<br>time of verification, in order to confirm that refrigerant used for the existing one<br>replaced by the project is prevented from being released to the air. |  |  |  |

### E. Emission Sources and GHG types

| Reference emissions                                |                 |  |  |  |
|--|-----------------|--|--|--|
| Emission sources GHG types                         |                 |  |  |  |
| Power consumption by reference chiller         CO2 |                 |  |  |  |
| Project emissions                                  |                 |  |  |  |
| Emission sources GHG types                         |                 |  |  |  |
| Power consumption by project chiller               | CO <sub>2</sub> |  |  |  |

### F. Establishment and calculation of reference emissions

#### F.1. Establishment of reference emissions

Reference emissions are calculated by multiplying power consumption of project chiller, ratio of COPs for reference/project chillers, and CO<sub>2</sub> emission factor for electricity consumed. The COP of reference chiller is conservatively set as a default value in the following manner to

ensure the net emission reductions.

1. The COP value tends to increase as the cooling capacity becomes larger.

- 2. The reference COP, which has a certain cooling capacity, is set at a maximum value in corresponding cooling capacity range.
- 3. The maximum values of COP in each cooling capacity ranges are defined as  $\text{COP}_{\text{RE},i}$  as described in Section I.

### F.2. Calculation of reference emissions

$$RE_{p} = \sum_{i} \{ EC_{PJ,i,p} \times \left( COP_{PJ,tc,i} \div COP_{RE,i} \right) \times EF_{elec} \}$$

REp: Reference emissions during the period p [tCO2/p]ECPJ,i,p: Power consumption of project chiller i during the period p [MWh/p]COPPJ,tc,i: COP of project chiller i calculated under the standardizing temperature conditions [-]

 $COP_{RE,i}$  : COP of reference chiller *i* under the standardizing temperature conditions [-]

EF<sub>elec</sub> : CO<sub>2</sub> emission factor for consumed electricity [tCO<sub>2</sub>/MWh]

## G. Calculation of project emissions

$$PE_{p} = \sum_{i} (EC_{PJ,i,p} \times EF_{elec})$$

 $PE_p$  : Project emissions during the period p [tCO<sub>2</sub>/p]

 $EC_{PJ,i,p}$  : Power consumption of project chiller *i* during the period *p* [MWh/p]

EF<sub>elec</sub> : CO<sub>2</sub> emission factor for consumed electricity [tCO<sub>2</sub>/MWh]

#### H. Calculation of emissions reductions

| $\mathbf{ER}_{\mathbf{p}} = \mathbf{RE}_{\mathbf{p}} - \mathbf{PE}_{\mathbf{p}}$ |   |  |  |  |
|--|---|--|--|--|
| ER <sub>p</sub>  | : Emission reductions during the period $p$ [tCO <sub>2</sub> /p] |  |  |  |
| REp  | : Reference emissions during the period $p$ [tCO <sub>2</sub> /p] |  |  |  |
| PEp  | : Project emissions during the period $p [tCO_2/p]$               |  |  |  |

# I. Data and parameters fixed *ex ante*

The source of each data and parameter fixed *ex ante* is listed as below.

| Parameter          | Description of data   | Source  |
|--------------------|---|---|
| EF <sub>elec</sub> | CO <sub>2</sub> emission factor for consumed electricity.             | [Grid electricity]                            |
|                    |   | The most recent published value               |
|                    | When project chiller consumes only grid                               | by the Ministry of Environment                |
|                    | electricity or captive electricity, the project                       | of Cambodia at the time of                    |
|                    | participant applies the CO <sub>2</sub> emission factor respectively. | validation.                                   |
|                    |   | [Captive electricity]                         |
|                    | When project chiller may consume both grid                            | For the option (a)                            |
|                    | and captive electricity, the project participant                      | Specification of the captive                  |
|                    | applies the CO <sub>2</sub> emission factor with lower                | power generation system                       |
|                    | value.  | provided by the manufacturer                  |
|                    |   | $(\eta_{elec,CG} [\%]).$                      |
|                    | In case the captive electricity is generated by                       | CO <sub>2</sub> emission factor of the fossil |
|                    | renewable energy source(s) and the amount of                          | fuel type used in the captive                 |
|                    | the captive electricity generated by the                              | power generation system                       |
|                    | renewable source(s) estimated from its                                | $(EF_{fuel,CG} [tCO_2/GJ])$                   |
|                    | generation capacities is equal to or less than                        |   |
|                    | half of the total electricity consumption at the                      | For the option (b)                            |
|                    | project site, the portion of electricity generated                    | Generated and supplied                        |
|                    | by the renewable source(s) may be neglected in                        | electricity by the captive power              |
|                    | the calculation of the captive $\text{CO}_2$ emission                 | generation system (EG <sub>PJ,CG,p</sub>      |
|                    | factor. If the amount of captive electricity                          | [MWh/p]).                                     |
|                    | generated by renewable source(s) is more than                         | Fuel amount consumed by the                   |
|                    | half, the captive $CO_2$ emission factor is                           | captive power generation system               |
|                    | determined by the following option (b) of "(2)                        | (FC <sub>PJ,CG,p</sub> [mass or volume/p]).   |
|                    | For captive electricity" using the total amount                       | Net calorific value (NCV $_{fuel,CG}$         |
|                    | of captive electricity generated by both fossil                       | [GJ/mass or volume]) and CO <sub>2</sub>      |
|                    | fuel and renewable sources for $EG_{PJ,CG,p}$ .                       | emission factor (EF <sub>fuel,CG</sub>        |
|                    |   | [tCO <sub>2</sub> /GJ]) of the fuel consumed  |
|                    | [CO <sub>2</sub> emission factor]                                     | by the captive power generation               |
|                    | (1) For grid electricity  | system in order of preference:                |
|                    | The most recent value available from the                              | 1) values provided by the fuel                |
|                    | source stated in this table at the time of                            | supplier;                                     |

#### validation is applied.

(2) For captive electricity
 Option (a) Calculated from its power generation efficiency (η<sub>elec,CG</sub> [%]) obtained from manufacturer's specification
 The power generation efficiency based on lower heating value (LHV) of the captive power generation system from the manufacturer's specification is applied;

$$\mathrm{EF}_{\mathrm{elec}} = 3.6 \times \frac{100}{\eta_{\mathrm{elec,CG}}} \times \mathrm{EF}_{\mathrm{fuel,CG}}$$

Option (b) Calculated from measured data The power generation efficiency calculated from monitored data of the amount of fuel input for power generation (FC<sub>PJ,CG,p</sub>) and the amount of electricity generated (EG<sub>PJ,CG,p</sub>) during the monitoring period p is applied. The measurement is conducted with the monitoring equipment to which calibration certificate is issued by an entity accredited under national/international standards;

 $EF_{elec} = FC_{PJ,CG,p} \times NCV_{fuel,CG} \times EF_{fuel,CG}$ 

$$\times \frac{I}{EG_{PJ,CG,p}}$$

Where:

NCV<sub>fuel,CG</sub>: Net calorific value of fuel consumed by the captive power generation system [GJ/mass or volume]

#### Note:

In case the captive electricity generation system meets all of the following conditions, the value in the following table may be applied to  $EF_{elec}$  depending on the consumed fuel type.  2) measurement by the project participants;
 3) regional or national default values;

4) IPCC default values provided in tables 1.2 and 1.4 of Ch.1Vol.2 of 2006 IPCC Guidelines on National GHG Inventories.Lower value is applied.

[Captive electricity with diesel fuel] CDM approved small scale methodology: AMS-I.A.

[Captive electricity with natural gas]

2006 IPCC Guidelines on National GHG Inventories for the source of EF of natural gas. CDM Methodological tool baseline "Determining the efficiency of thermal or electric generation energy systems version02.0" for the default efficiency for off-grid power plants.

|                     | <ul> <li>The system is non-renewable generation system</li> <li>Electricity generation capacity of the system is less than or equal to 15 MW</li> <li>fuel type</li> <li>Diesel fuel</li> <li>Natural gas</li> <li>EF<sub>elec</sub></li> <li>0.8 *1</li> <li>0.46 *2</li> <li>*1 The most recent value at the time of</li> </ul>  |   |                                |                                  |  |
|---------------------|--|---|--------------------------------|----------------------------------|--|
| COP <sub>RE,i</sub> | <ul> <li>validation is applied.</li> <li>*2 The value is calculated with the equation in the option (a) above. The lower value of default effective CO<sub>2</sub> emission factor for natural gas (0.0543 tCO<sub>2</sub>/GJ), and the most efficient value of default efficiency for off-grid gas turbine systems (42%) are applied.</li> <li>The COP of the reference chiller <i>i</i> is selected from the default COP values in the following table in line with cooling capacity of the project chiller <i>i</i>.</li> </ul> |   |                                |                                  |  |
|                     | /unit ≤3<br>(USRt)   | $\begin{array}{c c} 0 \leq x \\ 350 \\ 46 \\ 5.76 \\ \end{array}$ | 550 <x<br>≤750<br/>5.90</x<br> | 750 <x<br>≤1,300<br/>6.03</x<br> | The default COP value is<br>derived from the result of survey<br>on COP of chillers from<br>manufacturers that has high<br>market share. The survey should<br>prove the use of clear<br>methodology. The COP <sub>RE,i</sub><br>should be revised if necessary |
| COP <sub>PJ,i</sub> | The COP of project chiller <i>i</i> under the project specific condition.  |   |                                |                                  | from survey result which is<br>conducted by JC or project<br>participants.<br>Specifications of project chiller <i>i</i><br>prepared for the quotation or<br>factory acceptance test data by   |

|                            |  | manufacturer                               |
|----------------------------|--|--|
| T <sub>cooling-out,i</sub> | Output cooling water temperature of project                | Specifications of project chiller <i>i</i> |
|                            | chiller <i>i</i> set under the project specific condition. | prepared for the quotation or              |
|                            |  | factory acceptance test data by            |
|                            |  | manufacturer                               |
| T <sub>chilled-out,i</sub> | Output chilled water temperature of project                | Specifications of project chiller <i>i</i> |
|                            | chiller <i>i</i> set under the project specific condition. | prepared for the quotation or              |
|                            |  | factory acceptance test data by            |
|                            |  | manufacturer                               |